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Solution processed InAs nanowire transistors as microwave switches
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We demonstrate the feasibility of using self-assembled InAs nanowire bottom-gated field-effect transistors as radio-frequency and microwave switches by direct integration into a transmission line. This proof of concept is demonstrated as coplanar waveguide (CPW) microwave transmission line, where the nanowires function as a tunable impedance in the CPW through gate biasing. The key to this switching capability is the high-performance, low impedance InAs nanowire transistor behavior with field-effect mobility of $\sim 300 \mathrm{~cm}^{2} / \mathrm{Vs}$, on/off ratio of $10^{3}$ and resistance modulation from only $50 \Omega$ in the full accumulation mode, to $\sim 50 \mathrm{k} \Omega$ when the nanowires are depleted of charge carriers. The gate biasing of the nanowires within the CPW , results in a switching behavior, exhibited by a $\sim 10 \mathrm{~dB}$ ehange in the transmission coefficient, $\mathrm{S}_{21}$, between the on/off switching states, over $5-33 \mathrm{GHz}$. This frequency range covers both the microwave and millimeter-wave bands dedicated to IoT and 5 G applications. Demonstration of these switches creates opportunities for new class of devices for microwave applications based on solution processed semiconducting nanowires.

## 1. Introduction

Printed electronics offers significant advantages over conventional processing for radiofrequency (RF), microwave, and mm-wave applications, enabling rapid maskless prototyping, low temperature processing, and high density integration of microwave elements on large-area, light-weight flexible substrates. ${ }^{[1]}$ Printable filters, ${ }^{[2]}$ antennas, ${ }^{[3]}$ true-time delay lines,[4] wearable frequency selective surfaces (FSSs), ${ }^{[5,6]}$ reconfigurable antennas, ${ }^{[7]}$ phase-arrays, ${ }^{[8]}$ and reflect arraysf9] have been realised, which can enable wireless sensors in internet of things (IoT) ${ }^{[10]}$ and high data rate mm-wave fifth generation (5G) communications.[11,12] Microwave switches are key to enable reconfigurable antennas, arrays and FSSs, to modify their radiation pattern, resonant frequency, and polarization.[13,14]
Solution processable nanomaterials permit the integration of semiconductors and conductors, using low-temperature and inexpensive processing capability while compatible with flexible substrates. Main classes of solution processable semiconducting materials are conjugated


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molecules, carbon nanotubes (CNTs), graphene flakes (GFs), and inorganic semiconducting nanoparticle inks, including semiconducting nanowires (NWs). Although organic semiconductors are the most convenient for solution based deposition, the low charge carrier mobility, $0,1-10 \mathrm{~cm}^{2} \mathrm{~V}^{-1} \mathrm{~s}^{-1}[15][16]$ of organic printed FETs results in very high device resistance from tens of $\mathrm{k} \Omega$ to $\mathrm{M} \Omega$, limiting their application in microwave circuits. Other materials, such as CNTs and GFs, require chemical functionalization to be solution processable, which degrades charge transport properties resulting in field-effect mobilities of $9-42 \mathrm{~cm}^{2} \mathrm{~V}^{-1} \mathrm{~s}^{-1}$ for CNTs ${ }^{[17-19]}$ and below $1.2 \mathrm{~cm}^{2} \mathrm{~V}^{-1} \mathrm{~s}^{-1}$ for $\mathrm{GFs} .{ }^{[20-22]}$ These low mobilities give rise to high channel resistances, thus making these materials less desirable for solution processable high performance microwave switches. The most promising class of materials are semiconducting single crystal NWs, such as $\mathrm{HI}-\mathrm{V}$ materials, that possess high charge carrier mobility in the range of hundreds to few thousand $\mathrm{cm}^{2} \mathrm{~V}^{-1} \mathrm{~s}^{-1},[23,24]$ and they do not require surface functionalization for ink formulations.

In this work, we focus on solution processable InAs NWs due to the high electron mobility, reaching $6500 \mathrm{~cm}^{2} \mathrm{~V}^{-1} \mathrm{~s}^{-1}$ at room temperature, ${ }^{[25]}$ and low contact resistance with metal tracks, ${ }^{[26-28]}$ thereby avoiding the very resistive Schottky barriers common with other semiconducting NWs. ${ }^{[29]}$ Additionally, InAs has high electron affinity of $4.9 \mathrm{eV}^{[30]}$ and Fermi level pinning near the minimum of the conduction band, ${ }^{[31,32]}$ which helps to fabricate devices with excellent Ohmic contacts. However, Fermi level pinning can cause surface states impacting the on/off ratio and sub-threshold swing in FET devices. ${ }^{[30]}$ Regardless of the issues caused by the surface states, common for all semiconducting NWs, InAs nanowires have been shown to be C

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excellent candidates for high frequency FETs, in amplifier configuration, as they have reached a cut-off frequency of 103 GHz and maximum oscillation frequency of 155 GHz . ${ }^{[33]}$


## 2. InAs NW FET coplanar waveguide switch <br> 2.1. The concept of the switch

This paper presents a solution processed coplanar waveguide microwave switch, based on high performance InAs nanowires operating from 5 to 33 GHz . Switching is accomplished by driving $\sim 1000$ InAs nanowires between depletion high resistance state ( $>50 \mathrm{k} \Omega$ ), when the nanowires are practically imperceptible to the microwaves, and the accumulation low resistance state $(\sim 50 \Omega)$, where there is significant absorption of the microwave signal by the nanowires, resulting in $\sim 10 \mathrm{~dB}$ signal transmission variation between the 'on' and 'off' states.


A coplanar waveguide (CPW) was chosen as basis for the nanowire-based microwave switch as the frequency response of CPW with parasitic capacitances associated with field-effect transistor device structure is superior to that of microstrip design. The CPW has a center conductor and two outer grounded conductors that all support travelling electromagnetic (EM) waves (see Figure-1a).

### 2.2. InAs nanowire switch

To create the nanowire-based switch, it is important to have a very low channel resistance in the 'on' state, and correct switch dimensions to provide close to $50-\Omega$ characteristic impedance. Very low ohannel resistance, coupled with high on/off current ratio is a significant challenge for This article is protected by copyright. All rights reserved.

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solution processed nanowire FETs, and it has been addressed in the device design described below.

The gaps in the CPW device were bridged with single crystalline InAs NWs, built on top of a doped Si wafer with $1.5 \mu$ m thick silicon oxide $\left(\mathrm{SiO}_{2}\right)$ layer, as illustrated in Figure 1a. The $\mathrm{Si} / \mathrm{SiO}_{2}$ wafer provides a convenient substrate for the initial demonstration of the NW FET microwave switch as the fabrication processes on $\mathrm{Si} / \mathrm{SiO}_{2}$ are well developed for nanowires, and the doped Si acts as a common gate for the nanowire-based FET device. To achieve a low FET channel resistance, the gaps between the center conductor and grounds were designed to be 2.5 $\mu \mathrm{m}$. The signal line and ground line widths are 6 and $20 \mu \mathrm{~m}$ wide respectively. To accommodate conventional microwave ground-signal-ground measurement probes with $150 \mu \mathrm{~m}$ spacing, tapered lines were designed to connect to the CPW as shown in Figure 1b. The section between the dashed lines, included in Figure 1b, indicates the $500 \mu \mathrm{~m}$ long nanowire FET region of the switch. The dashed lines also indicate the references planes for the $S$-parameter measurements. Figure 1c shows an SEM image of the self-assembled NWs in the CPW, where the nanowires were deposited from dispersions in anisole, using an electric-field assisted dielectrophoresis (DEP) process.[23,34] The total number of NWs in the device is estimated to be $\sim 1000$ and though their distribution is not homogeneous, the length of the CPW $(l=500 \mu \mathrm{~m})$ is much smaller than the wavelength $(\lambda \approx 11.5 \mathrm{~mm}$ ) of the microwave signal (at 26 GHz ), so should not affect the device performance. A scanning-electron-microscopy (SEM) image is presented in Figure 1c, showing the 50 nm diameter InAs NWs bridging the gaps of the CPW.


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Figure 1. a) An illustration of the nanowire-based switch, showing the coplanar waveguide with central signal line and two ground lines bridged by nanowires. By applying a DC gate voltage (Vgs) to the common-gate $p^{++-S i}$ substrate, the nanowire transistor channel is driven between accumulation, low resistance state (positive $V_{g s}$ ), and depletion, high resistance (negative $V_{g s}$ ) state. Biasing circuit connections used to conduct full FET DC characterization are shown in the middle, with ground lines of CPW serving as FET source contacts, and the conductor line serving as FET drain Contact. RF characterization was conducted at different DC bias voltages applied to the gate, and two microwave ground-signal-ground probes were connected to port 1 and port 2 respectively. Reflected and transmitted signals were measured at port 1 and port 2 using vector network analyzer, when the gate voltage drives the FET between depletion and accumulation. b) Optical microscope image of the CPW switch with InAs NWs assembled in the gaps of the CPW and the tapered lines. The width of the signal and ground lines are $6 \mu \mathrm{~m}$ and $20 \mu \mathrm{~m}$ respectively. The length of the CPW forming the switch is $500 \mu \mathrm{~m}$, as indicated between the dashed lines. Tapers at the ends of the CPW were made for the microwave probes. c) SEM image of InAs NWs in the 2.5 um


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CPW gaps. d) STEM image of the InAs NW in the middle of the NW. e) indexed FFT of the corresponding areas marked areas in (d).


The diameter and crystal structure of the InAs NWs were investigated using scanning transmission electron microscopy (STEM) analysis (Figure 1d) and the corresponding fast Fourier transformations (FFTs) (Figure 1e). As reported previously, ${ }^{[35]}$ the length of the InAs NWs have fault-free stacking WZ structures, except for the seeded tip, which exhibits a zinc blend (ZB) due to post-growth cooling. The diameter of the InAs NWs was 50 nm with a native oxide layer <5 nm. More detailed TEM analysis is presented in Supporting Information. The specific fabrication steps of nanowire-based switch devices are provided in Experimental Section.

For high-frequency characterization of the switches, 2-port scattering parameters (Sparameters) were measured using a vector network analyzer (VNA) (Experimental Section). The S-parameters represent the ratio of the incident to outgoing waves at the ports of the device. The reflection coefficient of port 1 is denoted by $S_{11}$ and the transmission coefficient from port 1 towards port 2 is denoted by $S_{21}$.

Under zero or negative gate bias conditions, the conductance of the nanowires is very low and the NWs have minimal effect in the CPW transmission line performance, resulting in a low $\mathrm{S}_{11}$ and a high $\mathrm{S}_{21}$. In this paper these conditions will be referred to as "FET is OFF" and "closed state" of the switch.


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Under a positive and increasing gate bias, the conductance of the NWs increases, and their resistance is reduced. This results in a decreasing impedance between the signal and ground lines of the CPW line, resulting in an increase in the reflection and a decrease in the transmission coefficients of the switch. This condition will be referred to as "FET is ON" and "open state" of the switch.


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### 2.3. InAs NW FETs DC performance

To evaluate initial DC performance of the InAs NW-based switch, transistor characterization was performed using an Agilent 2902B analyzer under a dry nitrogen purge, at the same gate biasing voltages, as used for gate bias in microwave characterization ( $V_{\mathrm{gs}}$ from -60 to 100 V ).

Considering this FET as classical MOSFET operating in the linear regime,[36] the field-effect mobility $\mu_{\text {eff }}$ can be calculated as: [37]
$\mu_{\mathrm{eff}}=g_{\mathrm{m}} \frac{1}{V_{\mathrm{sd}}} \frac{L_{c h}^{2}}{C_{\mathrm{ox}}}$
where $\mu_{\mathrm{eff}}, g_{m,}, \mathcal{C}_{o x,} V_{s d}$ and $L_{c h}$ are field-effect mobility, transconductance $g_{m}=\left.\left(\frac{\partial I_{s d}}{\partial V_{s g}}\right)\right|_{V_{s d}}$, gate capacitance, source-drain voltage and transistor channel length, respectively. Calculation of the $\mathrm{C}_{\text {ox }}$ requires cylinder-on-plate model expression given by: ${ }^{[38]}$


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$C_{\mathrm{ox}}=N \frac{2 \pi \varepsilon_{0} \varepsilon_{\mathrm{r}, \mathrm{eff}} L_{\mathrm{ch}}}{\cosh ^{-1}\left(\frac{R_{\mathrm{NW}}+t_{\mathrm{ox}}}{R_{\mathrm{NW}}}\right)}$
where $\varepsilon_{0}=8.85 \cdot 10^{-12} \mathrm{~F} \mathrm{~m}^{-1}, \varepsilon_{\mathrm{r}, \text { eff }}, R_{\mathrm{NW}}=25 \mathrm{~nm}, N \sim 1000$ and $t_{\mathrm{ox}}=1.5 \mu \mathrm{~m}$ are vacuum permittivity, effective dielectric constant of $\mathrm{SiO}_{2}$ and air, radius of NW, number of NWs in the channel and oxide thickness, respectively. For nanowires positioned on top of gate dielectrics, the effective dielectric constant $\varepsilon_{\mathrm{r}, \text { eff }} \approx 2.2$ has been used, to take into account that nanowires are not embedded in the $\mathrm{SiO}_{2}$ layer.[38]

The transfer characteristics of a typical InAs NW FET are shown in Figure 2 and demonstrate ntype transport, with full depletion of the FET channel achievable at $V_{\text {sg }}$ from -60 to -40 V , and full accumulation of the FET at $V_{\text {sg }}$ from 60 to 100 V . Switching the transistor between ON and OFF states (accumulation/depletion) provides InAs nanowire FETs on/off current ratio of $\sim 10^{3}$. The transconductance is plotted in the inset (of Figure 2 a ), and its peak value is $\approx 6 \mu \mathrm{~S}$ at $\mathrm{V}_{\mathrm{sg}}=0 \mathrm{~V}$ and $V_{s d}=20 \mathrm{mV}$. Also, from the linear part of the sub-threshold region of the transfer plot, the sub-threshold swing, $S S \equiv\left(\frac{\partial \log I_{s d}}{\partial V_{s d}}\right)^{-1}$, is approximately $10 \mathrm{~V} / \mathrm{dec}$. By using equations (1-2) field-effect mobility was estimated to be $\sim 300 \mathrm{~cm}^{2} \mathrm{~V}^{-1} \mathrm{~S}^{-1}$. The output characteristics of InAs nanowire FETs (Figure 2b) exhibit linear behavior over the entire source-drain voltage measurement range, confirming the Ohmic properties of the contacts. The FET ON-state resistance was estimated to be $\approx 50 \Omega$ from the inverse gradient of the I-V curve $\left(\mathrm{V}_{\mathrm{sg}}=100 \mathrm{~V}\right)$, demonstrating $I_{\text {sd }}$ of 2 mA at $V_{\text {sd }}$ of 100 mV .


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Figure 2. a) DC transfer characteristics of the assembled InAs nanowire-based switch, on a linear scale. Inset shows FET characteristics on a log-linear scale (red line) and transconductance vs gate voltage (black line). b) DC output characteristics of the NW-based FET switch, with 50 Ohm device resistance obtained in full accumulation regime (Vsg=100V).

### 2.4. InAs NW FETs switch RF/microwave performance

The same FET devices were then used for microwave characterization (Experimental Section).

Initially, to evaluate the possible influence of the highly doped $\mathrm{p}^{++}$-Si substrate (resistivity of 0.1 $\Omega \mathrm{cm}$ ), S-parameters of the CPW with full transistor geometry, but without semiconducting nanowires were performed. The back gate ( $\mathrm{p}^{++}-\mathrm{Si}$ ) was biased at the same levels as during FET tests. The measurements confirmed that at $-60,0$ and 100 V gate bias, the S-parameters of the structures, without nanowires, do not show evident changes. (Supporting Information). Thus, it was concluded that biasing effects of the conducting Si common gate can be neglected.


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S-parameters of the InAs NW FET devices were measured up to 33 GHz and the results are presented in Figure 3. Reflection, $\mathrm{S}_{22}$ (Figure 3a), and transmission, $\mathrm{S}_{21}$ (Figure 3b), coefficients in dB-scale represent the operation of the switch at high frequencies. Both the reflection and transmission coefficients change significantly when the switch is closed (negative $V_{\text {sg }}$ ) and open (positive $V_{\text {sg }}$ ). When the gate bias is negative (FET is depleted), the resistance of the nanowires is two orders of magnitude larger than the characteristic impedance and it should not affect Sparameters. Indeed, when the gate bias is negative: (i) transmission remains high, giving $S_{21}$ in the range between -4 dB and -2 dB ; (ii) reflection remains low with $\mathrm{S}_{22}$ below -20 dB ; (iii) S parameters do not change at $V_{\text {sg }}$ of $-60,-40$ and -20 V . It indicates that signal is transmitted and the switch is closed. Note that the resistance is estimated to be $\approx 128 \Omega$ when gate bias is zero (calculated as an inverse gradient of the I-V curve at $V_{s g}=0 \mathrm{~V}$ ), and S-parameters did not change significantly as compared to the closed switch conditions.

The behavior of $S$-parameters changes when $V_{\text {sg }}$ is more positive - transmission decreases and reflection-increases, turning the switch into an open state. The strongest effect happens at $V_{\text {sg }}$ $=100 \mathrm{~V}$ when the channel resistance is $\approx 50 \Omega$, i.e. $\mathrm{S}_{21}$ drops by 7-10 dB, indicating low transmission, and $S_{22}$ varies between -13 dB and -6 dB , indicating an increase in reflection.

In regards to the range of gate voltages producing the majority of switching effect, it was observed that relatively modest voltages, $\mathrm{V}_{\text {sg }} \sim-5 \mathrm{~V}$ were sufficient to keep the switch in the closed state, to allow microwave transmission, whereas positive gate voltage at the level of $\sim 60 \mathrm{~V}$ have provided strong reflection characteristics, corresponding to the switch open state. Additional modelling using Sonnet EM planar electromagnetic simulator based on method-of?

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moments have shown that currently used $1.5 \mu$ m thickness of $\mathrm{SiO}_{2}$ gate dielectric can be reduced to $0.3 \mu \mathrm{~m}$ thickness, without sacrificing the performance of the switch. Such 5 -fold dielectric thickness reduction is expected to bring about corresponding decrease of gate voltages to 1520V level.

S-parameters of the switch can be described by a transmission line model having an additional variable shunt admittance (Figure 3f), i.e. the NWs between the signal and ground lines of the CPW add a shunt admittance, $Y_{N W}$. This admittance is composed of the NW conductance and associated inductance. Hence, $Y_{N W}=G_{N W}-i / \omega L_{N W}$, where $G_{N W}$ and $L_{N W}$ are the distributed conductance and inductance, respectively, whose values are controlled by the gate bias applied to the NWFETs. The characteristic impedance, $Z_{0}$, and propagation constant, $\gamma$, of the CPW line, with the nanowires, can be defined as: ${ }^{39]}$
$Z_{0}=\sqrt{\frac{Z}{Y+Y_{\mathrm{NW}}}}$
$\gamma=\alpha+i \beta=\sqrt{Z\left(Y+Y_{\mathrm{NW}}\right)}$
where $Z=R+i \omega L$ and $Y=G+i \omega C, R, L, G$ and $C$ are the distributed resistance, inductance, conductance, and capacitance of the unloaded CPW (per unit length), $\alpha$ and $\beta$ are attenuation and phase constant, respectively. The attenuation is the loss in the transmission line as the electromagnetic wave propagates and $Z_{0}$ is the characteristic impedance. Both $Z_{0}$ and $\alpha$ can be calculated from S-parameters via ABCD parameters ${ }^{[39]}$ as described in Supporting Information.

Using Equations (S6) and (S7), (Supporting Information), $\alpha$ and $\operatorname{Re}\left(Z_{0}\right)$ are plotted in Figure


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$3(c, d)$. As the gate bias is increased and positive (FET is 'on') InAs NWs channel becomes more conductive, i.e. the shunt conductance $G_{N W}$ increases. This gives rise to an increased attenuation constant, indicating an increase in loss associated with NWs. Therefore, the transmission coefficient, $S_{21}$, decreases. Furthermore, according to Equation (3), $Z_{0}$ also changes resulting in a mismatch with the nominal $50 \Omega$ at the reference plane, and therefore input reflection of the switch, $S_{11}$, will inerease; which further decreases the signal that passed through the switch.

It is interesting to determine the values of the NW conductance, $G_{\mathrm{NW}}$, and inductance, $L_{\mathrm{NW}}$ at microwave frequencies. These values can be obtained by noting that:


We see from equation (6) that the ratio $\gamma / Z_{0}$ gives the sum of the unloaded distributed shunt admittance of the CPW transmission line, $Y$, and the additional contribution from the NWs, $Y_{\mathrm{NW}}$. The value of $Y$ can be determined by measuring the CPW with no NWs (or this case, the CPW line with NWs but very large negative $V_{\text {sg }}$ - resulting in $\mathrm{Y}_{\mathrm{NW}}=0$ ). The value of Y then follows from equation (6) with $\mathrm{Y}_{\mathrm{NW}}=0$ and equations (S6) and (S7). The measurements are then repeated for a CPW line with NWs resulting in $\gamma / Z_{0}$ from equation (6). Therefore, if we find the difference between these loaded and unloaded values we can determine the additional distributed NW


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Figure 3 (e) shows the extracted values of $G_{\mathrm{NW}}$ using equations (S6) and (S7) (Supporting Information) and equation (7). It is seen that the NW conductance varies from approximately $0.06 \mathrm{~S} \mathrm{mn}^{-1}$ for $V_{\mathrm{sg}}=100 \mathrm{~V}$ reducing to a figure of $0.005 \mathrm{~S} \mathrm{~mm}^{-1}$ for $V_{\mathrm{sg}}=0 \mathrm{~V}$. Although not plotted for brevity, the inductance varies from 0.5 nH mm at $V_{\mathrm{sg}}=100 \mathrm{~V}$ up to 1.5 nH mm at $V_{\mathrm{sg}}=20 \mathrm{~V}$. Note that the unusual units of nH mm arise from the fact that the shunted NW admittance in equation (7), $Y_{\mathrm{NW}}$, has units of $\mathrm{Smm}^{-1}$. There is a frequency dependence for $G_{\mathrm{NW}}$ and $L_{\mathrm{NW}}$, with $G_{\mathrm{NW}}$ decreasing with frequency and $L_{\mathrm{NW}}$ increasing, as is in the case of a conducting wire due to the skin effect. The imaginary component of $Y_{\mathrm{NW}}$, due to $L_{\mathrm{NW}}$, is comparable in magnitude to the real part $G_{\mathrm{NW}}$ at lower frequencies; however, due to the $1 / \omega$ dependence, it becomes insignificant at 33 GHz . This explains the increase in $\operatorname{Re}\left(Z_{0}\right)$ for positive $V_{\mathrm{sg}}$ as the frequency increases.

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Figure 3 a,b) Reflection coefficient $S_{22}$ and transmission coefficient $S_{21}$ in dB scale at different $V_{\text {sg }}$ from -60 V to 100 V with a step of 20 V . Representation of the S -parameters in dB follows the formula $S_{i j}[d B]=20 \log S_{i j}$ where $i, j$ are 1 or $2 ;$. $c, d$ ) Attenuation, $\alpha$, and $\operatorname{Re}\left(\mathrm{Z}_{0}\right)$, calculated from S-parameters at respective $\mathrm{V}_{\text {sg }}$, e) Effective distributed NW conductance, f) Equivalent circuit diagram of CPW InAs NW switch.


Finally, the switch performance was demonstrated in an offset-open configuration that can be employed in a reconfigurable matching circuit based on single-stub tuning, thus providing additional capabilities for the design of reconfigurable microwave circuits based on phase shift. The devices yere implemented by assembling InAs nanowires at the terminating end of the CPW and have demonstrated very good performance with nanowire FET providing a variable resistive load ranging from $33 \Omega$ to $1.67 \mathrm{k} \Omega$, resulting in the phase shift of $180^{\circ}$ at 3 GHz . (SupportingInformation)

## 3. Conclusions

In summary, sofution processable InAs nanowire bottom-gated FETs were demonstrated as microwave switches working in the frequency range of 5 to 33 GHz . The large number of NWs, assembled in shunt configuration by dielectrophoresis, has enabled tuning of the overall resistance by 3 orders of magnitude from $\sim 50 \Omega$ to $\sim 50 \mathrm{k} \Omega$, where $50 \Omega$ NW FET resistance is the lowest reported among solution processed or direct transferred, planar NW FETs with lowk gate-dielectric, ${ }^{[40]}$ to the best of the authors' knowledge. For instance, solution processed multi-NW ZnO FETs with 300 nm thick parylene top-gate dielectric demonstrated ON-resistance of $\approx 0.5 \mathrm{M} \Omega_{\Omega}^{[37]}$ whereas bottom-gated Si NWs with 250 nm thick $\mathrm{SiO}_{2}$ dielectric exhibited ON-


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resistance of $13 \mathrm{k} \Omega .{ }^{[34]}$ Dense arrays of InAs NW FET with transfer printed nanowires on flexible substrate with $\sim 8 \mathrm{~nm}$ thick $\mathrm{Al}_{2} \mathrm{O}_{3}$ gate dielectric demonstrated ON-resistance of $1 \mathrm{k} \Omega$ with ON/OFF ratio ${ }^{[41]} 10$ times lower than the one reported in this work. In general, the majority of high-frequency III-V and, especially, InAs multi-NW FETs reported in the literature, are vertical structures ${ }^{[42]}$ fabricated by non-printed electronics deposition techniques.

The RF/microwave characterization of the switches demonstrated the difference in transmission and reflection coefficients between closed and open states of the switch to be 7-10 dB and 6-13 dB, respectively, though there were losses related to the $\mathrm{p}^{++}-\mathrm{Si}^{2} / \mathrm{SiO}_{2}$ substrate and thin, narrow conductors of the CPW. An isolation of around 10 dB is considered to be sufficient for reconfigurable devices, whereas microwave and millimeter-wave operation of the switches is particularly attractive for reconfigurable antennas/surfaces for wireless communications and IoT,[43] space applications, remote sensing, surveillance and beam-forming circuits. ${ }^{[44]}$ FET switch design offers several advantages, including very low power consumption as compared to PIN diodes, ${ }^{[45]}$ fast switching times and normal temperature operation as compared to phasechange temperature tunable switches $\left(\mathrm{GeTe}\right.$ and $\left.\mathrm{VO}_{2}\right)$.[46]

Finally, we demonstrated the switch in offset-open geometry, where it played the role of a phase shifter with a maximum phase shift of $180^{\circ}$ at 3 GHz .

To conclude, further improvements of InAs NWs FET microwave/mm-wave switches can be gained by replacing lossy silicon with low-loss plastic substrates and thinner low-k polymeric


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dielectrics to push up operating frequency range while reducing operating voltages and to move towards truly flexible electronics.


## 4. Experimental Section

Nanowiresigrowth and dispersions preparation: The InAs nanowires were grown via the vapor-liquid-solid mechanism using 30 nm diameter Au nanoparticles dispersed from a commercial colloidal Aut solution on a poly-L-lysine treated $\operatorname{InAs}(111) \mathrm{B}$ substrate by metal-organic vapor phase epitaxy (MOVPE). Growth was conducted in an Aixtron 200/4 reactor at 100 mbar hydrogen atmosphere with total flow rate of 15 slm, using trimethylindium and arsine as precursors. The nannowires were grown at $597{ }^{\circ} \mathrm{C}$ for 60 min with a $\mathrm{V} / \mathrm{III}$ ratio of 1.6 after 10 min of anrealing at $650{ }^{\circ} \mathrm{C}$ to remove the substrate native oxide and allow for alloying between the gold droplet and indium from the substrate. These conditions provided excellent growth yield, <111>B nanowire growth direction, and mainly stacking fault-free wurtzite crystal structure. ${ }^{[35]}$

Nanowires dispersions were obtained by sonicating as-grown InAs NWs in anisole to detach NWs from the host substrate. Typical length of the nanowires in the dispersion was 5-7 microns. Positive photolithography and lift-off technique were used for fabrication of metal tracks on the substrate. Bi-layertechnique of PMGI SF6 and S1805 photoresists was used.


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Bottom electrodes for DEP: Auxiliary Al bottom electrodes, 20nm thick, for dielectrophoresis, were structured by photolithographic lift-off technique.
$D E P$ was performed on an inclined substrate. ${ }^{[34]}$ Sinusoidal signal of $10 \mathrm{kHz}, 20 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ was applied to Al devide electrodes, and nanowires formulation was drop-casted on top. DEP was conducted for 30 sec. Excessive nanowires and clusters of nanowires were removed by quick device sonication in IPA. We note that more controllable positioning, orientation, nanowire-tonanowire spacing and nanowires density per unit area can be obtained by following DEP and impedance spectroscopy methodology demonstrated by us in Ref[34] where nanowires' selfassembly response to the DEP electric field, its strength and DEP signal frequency was studied in depth.

Top electrodes and sulfurization of the contacts: Before top-electrode deposition, nanowires under the contact area were treated with ammonium polysulfide solution for 10 min at $40^{\circ} \mathrm{C}$. The solution was prepared ${ }^{[47]}$ by adding of $150 \mu \mathrm{l}$ of $20-25 \%$ water solution of $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{~S}$ and $50 \mu \mathrm{l}$ of S-saturated $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{~S}_{\mathrm{x}}$ into 200 ml of DI water. The saturated component was prepared by adding 3 g of sulfur powder into 30 ml of $20-25 \%\left(\mathrm{NH}_{4}\right)_{2}$ S. Sulfurization process was stopped by rinsing the samples in DI water. Top contacts (Ti/Au), 150 nm thick, were deposited by e-beam samples evaporation and structured by lift-off technique.

Microwave characterization: Two-port S-parameters measurements were performed using a Keysight N5247A PNA-X network analyzer, MPI TS-2000 SE probe station, and two MPI Titan 26 GHz GSG probes both having a $150 \mu \mathrm{~m}$ pitch, used to contact the fabricated CPW switch. The


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shielded environment of the probe station was purged with nitrogen and kept at room temperature during the measurements. Measurements were performed from 5 to 33 GHz , at an input power of -10 dBm . Weak LED microscope light was used to allow positioning of microprobes onto the samples, with light intensity of $20-50 \mu \mathrm{~W} / \mathrm{cm}^{2}$. No detectable influence of microscope light was observed on either DC or frequency responses of the devices. This intensity level is approximately 3 orders of magnitude lower than previously reported light intensity of $30 \mathrm{~mW} / \mathrm{cm}^{2}$ used to study photoconductivity of InAs nanowires in Ref.[48]

On-wafer multiline thru-reflect-line (mTRL) calibration was performed to move the reference plane of the measurement to the CPW switches (end of the tapered lines). The standards used for the calibration were a zero-length 'thru', a 'reflect' and two 'lines' with lengths of $1350 \mu \mathrm{~m}$ (covering $5-26 \mathrm{GHz}$ ) and $450 \mu \mathrm{~m}$ (covering $25-65 \mathrm{GHz}$ ), in order to cover the desired frequency range. One additional 'line' structure of $2200 \mu \mathrm{~m}$ was built to cover frequencies between 3 and 24 GHz for the offset-open. The source-drain DC bias (Agilent 2902B) was applied to the devices through one of the bias tees of the VNA and one of the two GSG probes, whereas the gate DC bias was applied through an MPI Kelvin probe.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the corresponding author.


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Solution-processed microwave InAs nanowire switches are demonstrated with tuneable transmission/reflection of 10 dB at $5-33 \mathrm{GHz}$ frequency range for the next-generation of reconfigurable antennas and smart surfaces. The devices are based on nanowire FETs in coplanar waveguide configuration with InAs nanowires providing variable impedance through gate biasing, with ON/OFF ratio of $10^{3}$ and very low ON- resistance of $\sim 50 \Omega$.


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