# Dry-etch of As<sub>2</sub>S<sub>3</sub> thin films for optical waveguide fabrication

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Plasma etching to  $As_2S_3$  thin films for optical waveguide fabrication has been studied using a helicon plasma etcher. The etching effects using the processing gases or gas mixtures of  $O_2$ , Ar, and  $CF_4$  were compared. It was found that the O<sub>2</sub> plasma had no chemical etching effect to the As<sub>2</sub>S<sub>3</sub>, but it could oxidize the surface of the As<sub>2</sub>S<sub>3</sub>. The Ar plasma provided a strong ion sputtering effect to the films. The  $CF_4$  plasma exhibited a too strong chemical etch to the  $As_2S_3$ , leading to serious undercutting and very rough sidewalls of the waveguides. Ar and O<sub>2</sub> gases were compared as the additives to dilute the  $CF_4$  processing gas. The etch rate of the  $As_2S_3$  was reduced dramatically from over 2000 nm/min to a few hundred nm/min when the pure  $CF_4$  gas was heavily diluted with 70% Ar or  $O_2$  gas. The undercutting and sidewall roughness of the etched waveguides were also decreased greatly when above dilution was made, which was associated with an enormous weakening of the isotropic chemical etch induced by neutral reactants in the plasma. In addition, the  $O_2$  showed a better dilution effect than the Ar in reducing the etch rate of the As<sub>2</sub>S<sub>3</sub>; and the  $O_2/CF_4$ plasma also enabled a much lower erosion rate to Al mask layers than the  $Ar/CF_4$  plasma at similar plasma conditions. The  $As_2S_3$  waveguides with near vertical and very smooth sidewalls were obtained using an optimized  $O_2/CF_4$  plasma. Moreover, the etching behaviors and mechanisms were explained base on the etching results, and on the characteristics of the applied plasma diagnosed using Langmuir probe and optical spectroscopy techniques. © 2005 American Vacuum Society. [DOI: 10.1116/1.2049308]

## I. INTRODUCTION

Chalcogenide glasses possess third order optical nonlinearities more than 500 times higher than fused silica, with similar response times and favorable nonlinear figure of merit. They, therefore, can be used for fast all-optical processing, including all-optical multiplexing and demultiplexing; wavelength conversion; Raman and parametric amplification.<sup>1-3</sup> Chalcogenides form glasses over a wide range of compositions, allowing their refractive indexes to be tuned to obtain very high index contrast between the core and cladding of a waveguide. This makes single mode waveguides with small cross-sectional area and small bend radii achievable. As a result, low peak power (<1 W) alloptical processing is possible in planar waveguide structures fabricated in chalcogenide glasses. In addition, chalcogenides are also promising for magneto-optic devices, due to their moderate Verdet constants in the infrared.<sup>3</sup>

To realize their potential applications, the chalcogenides, need to be patterned into micro-sized low loss optical waveguides. Techniques for producing high-quality chalcogenide glass films, including thermal evaporation, sputtering, chemical vapor deposition, and pulsed laser deposition, have been well developed.<sup>4–6</sup> However, patterning the chalcogenide films into waveguides remains a difficulty. Laser-writing has been used to generate waveguides using the well-known photosensitivity of chalcogenides to light near their band edge.<sup>5,7</sup> The photo-induced refractive index change is, however, not stable in the long term due to relaxation of the structure, and is, therefore, unsuitable for devices. Wet-etch can also be used, but being an isotropic process serious undercutting of the mask always occurs making the control of waveguide dimensions difficult.<sup>5</sup> Recently, chalcogenide waveguides were fabricated using Ar-plasma etching.<sup>4</sup> The profile of the generated waveguides was, however, not rectangular due to a very poor etching selectivity between the chalcogenide glass and photoresist mask.

In this work, dry etching to  $As_2S_3$  chalcogenide glasses using CF<sub>4</sub>-based plasma was studied. It was found that the etch rate of  $As_2S_3$  by pure CF<sub>4</sub> plasma was extremely high, ~1.5-3 µm/min depending on the plasma power, making the control of the etch depth and waveguide profile very difficult, and thus the CF<sub>4</sub> gas needed to be diluted. O<sub>2</sub> and Ar gases were tested as the additive gases. The etching characteristics using different gases or gas mixtures of O<sub>2</sub>, Ar, and CF<sub>4</sub> were investigated and compared for a better understanding of the etching behavior and mechanism.

 $As_2S_3$  waveguides with near vertical and smooth sidewalls were achieved using an optimized  $CF_4/O_2$  plasma. The waveguides were shown to have a low loss of ~0.25 dB/cm at 1550 nm, and to be suitable for application in all-optical processing.<sup>8</sup> The waveguide fabrication process is fully compatible with mature silicon microelectronics fabrication methods, and thus is highly suitable for device production.

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## **II. EXPERIMENTS**

Thin films of the  $As_2S_3$  chalcogenide glasses were deposited on 4-in.-diameter silicon wafers using an ultrafast pulsed laser ablation technique (UFPLA).<sup>9</sup> This technique employs a frequency doubled mode-locked Nd:YAG laser producing 6–7 W average power (70–80 nJ/pulse) at 532 nm, at a repetition rate of 76 MHz. The technique has been proven to produce atomically smooth films free from particle contamination.

Before dry-etching, Al films of 300-400 nm thick were sputter-coated onto the samples and patterned to create etch resistant masks using standard photolithography and wet etching techniques. To prevent the Al films from peeling off during processing due to the mismatch of the thermal expansion coefficients of Al and As<sub>2</sub>S<sub>3</sub>, a thin (<100 nm) photoresist layer was usually spin-coated onto the As<sub>2</sub>S<sub>3</sub> surface prior to sputter-coating the Al mask layer.

Dry etching was carried out in a helicon plasma etcher, which is a high-density low-pressure plasma system.<sup>10</sup> It consists of two joined chambers, the source and diffusion chambers. The source chamber is a 15-cm-diameter, 25-cm-long glass tube surrounded by a "Boswell-type" helicon antenna and two solenoids. The diffusion chamber is a 30-cm-diameter and 30-cm-long aluminum cylinder surrounded by two additional solenoids. The currents in the 4 solenoids are adjusted to produce a magnetic field of 100 G in the source and 60 G in the diffusion chamber. The substrate holder is mounted at the bottom of the diffusion chamber, and is water-cooled. Both the source antenna and the substrate holder are driven by 13.56 MHz rf power sources. The chambers are pumped with an ATP 400 HPC turbomolecular pump. The processing gases (CF<sub>4</sub>, O<sub>2</sub>, and Ar) are admitted into the vacuum chamber through 3 separate mass flow controllers.

For diagnosing the plasma, a Langmuir probe was used to measure the ion saturation current at the substrate position. A -63 V dc voltage was applied to the probe tip to collect positive ions only. In addition, a *Monolite 6602* optical spectrum analyzer was used to measure the optical emission intensities of fluorine atoms at the wavelength of 684.6 nm. For all these diagnosing measurements, there was no rf power applied to the substrate.

The etch rates of the  $As_2S_3$  and the Al mask were measured *in situ* using an ellipsometer, or *ex situ* using a surface profilometer. The microprofiles of the waveguides were investigated under a field emission scanning electron microscopy (FESEM). The sidewall roughness of the waveguides was determined by measuring the average amplitude of the corrugations or ripples within a 2- $\mu$ m range on the sidewalls using the FESEM.

# **III. RESULTS AND DISCUSSIONS**

#### A. Characteristics of the plasma

To understand the plasma-etching behaviors to the  $As_2S_3$ films, the characteristics of the applied plasma were diagnosed using the Langmuir probe and the optical spectroscopy

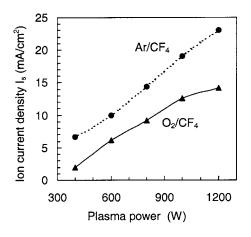


FIG. 1. Ion saturation current at the substrate location vs the plasma power for the gas mixtures of  $Ar/CF_4=7/3$  and  $O_2/CF_4=7/3$ . The pressure was 10 mTorr, and the substrate was not biased.

techniques. Figure 1 shows the dependencies of the ion saturation currents ( $I_s$ ) at the wafer location on the plasma power (P) for the gas mixtures of Ar/CF<sub>4</sub> and O<sub>2</sub>/CF<sub>4</sub>. The gas flow rates were 70 sccm for both Ar and O<sub>2</sub>, and 30 sccm for CF<sub>4</sub>, the gas pressure was kept at 10 mTorr, and no substrate rf bias was applied. As seen in Fig. 1,  $I_s$  increases almost linearly with P for both the Ar/CF<sub>4</sub> and O<sub>2</sub>/CF<sub>4</sub> gas mixtures, indicating the ion and electron densities increase with P. It is also seen in the figure that the  $I_s$  of the Ar/CF<sub>4</sub> plasma is obviously much higher than that of the O<sub>2</sub>/CF<sub>4</sub> plasma at the same P. This is caused by the fact that Ar gas has much higher ionization efficiency in the plasma than the electronegative O<sub>2</sub> gas.

Figure 2 shows the variations of  $I_s$  versus the Ar/CF<sub>4</sub> and O<sub>2</sub>/CF<sub>4</sub> gas flow ratios, which were measured at P=600 W and pressure 10 mTorr. As shown here,  $I_s$  increases slightly, but decreases, with the increase of the Ar/CF<sub>4</sub> or O<sub>2</sub>/CF<sub>4</sub> gas flow ratio, respectively.

In addition, the dependence of  $I_s$  on the plasma pressure was measured at P=600 W for both the gas mixtures of Ar/CF<sub>4</sub>=7/3 and O<sub>2</sub>/CF<sub>4</sub>=7/3. The results are displayed in Fig. 3. It is seen here that for both the gas mixtures,  $I_s$  in-

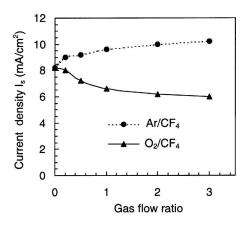


FIG. 2. Ion saturation current vs the gas flow ratio of  $Ar/CF_4$  or  $O_2/CF_4$ . The plasma power was 600 W, pressure 10 mTorr, and the substrate was not biased.

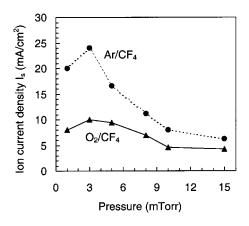


FIG. 3. Variation of the ion saturation current with the plasma pressure for the gas mixture of  $Ar/CF_4=7/3$  or  $O_2/CF_4=7/3$ . The plasma power was 600 W, and the substrate was not biased.

creases when reducing the pressure from 15 to 3 mTorr, reaches a maximum at  $\sim$ 3 mTorr, and then decreases with further reduction of the pressure.

In order to get the information about the concentration of the reactive species in the plasma, the optical emission intensity of the atomic F ( $I_F$ ) at the wavelength of 684.6 nm was measured. The  $I_F$  depends on the concentration of the F atoms dissociated from the CF<sub>4</sub>, and on the excitation efficiency of the plasma to the F atoms. Therefore  $I_F$  is related to the dissociation ratio of the CF<sub>4</sub> gas, and it also indirectly reflects the density of other species (CF, CF<sub>2</sub>, CF<sub>3</sub>), since the more F atoms are dissociated from the CF<sub>4</sub>, the more other species are generated at the same time.<sup>11</sup> The excitation efficiency is related to plasma density, especially the electron density, since the electrons are the main source to excite the F atoms.

The variation of  $I_F$  versus the plasma power *P* was plotted in Fig. 4. The gas mixtures were also Ar/CF<sub>4</sub>=7/3 and O<sub>2</sub>/CF<sub>4</sub>=7/3, and the plasma pressure 10 mTorr. As seen in Fig. 4,  $I_F$  increases almost linearly with *P*, and the  $I_F$  for the Ar/CF<sub>4</sub> plasma is obviously much higher than that of the

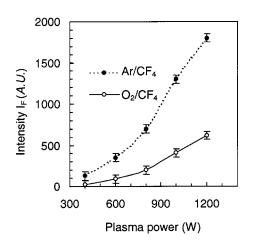


FIG. 4. Optical emission intensity of atomic F at the wavelength of 684.6 nm as a function of plasma power for the gas mixture of  $Ar/CF_4=7/3$  or  $O_2/CF_4=7/3$ . The pressure was 10 mTorr, and the substrate was not biased.

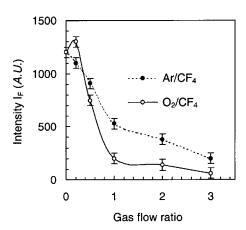


FIG. 5. Optical emission intensity of atomic F at the wavelength of 684.6 nm as functions of the gas flow ratios of  $Ar/CF_4$  and  $O_2/CF_4$ . The plasma power was 600 W, pressure was 10 mTorr, and the substrate was not biased.

 $O_2/CF_4$  plasma at the same *P*. Here the increase of  $I_F$  with *P* should be associated with the increase of the dissociation ratio of the CF<sub>4</sub>, and to the increase of the excitation efficiency of the F atoms. In addition, the reason of the higher  $I_F$  of the Ar/CF<sub>4</sub> than the  $O_2/CF_4$  plasma should be related mainly to a higher excitation efficiency of the atomic F in the Ar/CF<sub>4</sub> plasma, because of the higher plasma density of the Ar/CF<sub>4</sub> gas mixture than the  $O_2/CF_4$ , as evidenced by the results in Fig. 1.

The dependencies of  $I_{\rm F}$  on the Ar/CF<sub>4</sub> and O<sub>2</sub>/CF<sub>4</sub> gas flow ratios are illustrated in Fig. 5. Here P was kept at 600 W, and gas pressure was 10 mTorr. It is seen in Fig. 5,  $I_{\rm F}$  decreases all the way with the increase of Ar/CF<sub>4</sub> gas flow ratio; but for the  $O_2/CF_4$  gas mixture,  $I_F$  exhibits an initial rise when the ratio increases to  $\sim 0.2$ , and then it drops down quickly with further increase of the  $O_2/CF_4$  ratio. It is known that oxygen could react with  $CF_x$  radicals in the plasma, producing carbon oxides (CO,CO<sub>2</sub>) and atomic  $\mathbf{F}^{11,12}$  This could be the reason for the initial increase of the  $I_{\rm F}$ . However, this effect was counterbalanced by further diluting effect of the  $O_2$  addition, so that  $I_{\rm F}$  dropped down at higher O<sub>2</sub>/CF<sub>4</sub> ratio. The excitation efficiency of the F atoms should not change much with the variation of the gas ratio at the same plasma power, since the plasma density did not change much with the gas ratio at constant P, as evidence by the results in Fig. 2. Therefore, we can judge form Fig. 5, the concentration of atomic F was enormously diluted by increasing the Ar/CF<sub>4</sub> or  $O_2/CF_4$  flow ratio to over 2/1, and at the same time, the concentration of other radicals  $(CF, CF_2, CF_3)$  dissociated from the  $CF_4$  should be also greatly reduced when above dilution was made.

## B. Etch rate and selectivity

To check the chemical etching effect of different processing gas or gas mixtures  $(O_2, Ar, CF_4, Ar/CF_4, O_2/CF_4)$ , their etching rates to the  $As_2S_3$  were tested without applying rf bias to the substrate for reducing the ion bombardment effect of the plasma. The results were list in Table I. The applied plasma power was 600 W, and pressure 10 mTorr for all the

TABLE I. Etch rate of  $As_2S_3$  films floated in different plasma with a power of 600 W.

Sample	Gas flow (sccm)	Etch time (min)	Etch rate (nm/min)
1	O <sub>2</sub> =70	10	0
2	Ar=70	10	20
3	CF <sub>4</sub> =90	2	1500
4	CF <sub>4</sub> /Ar=30/70	2	210
5	$CF_4/O_2 = 30/70$	2	130
6 <sup>a</sup>	$CF_4/O_2 = 30/70$	2	20
7 <sup>b</sup>	$CF_4/O_2 = 30/70$	2	100

<sup>a</sup>The sample surface was preoxidized in an O<sub>2</sub>-plasma.

<sup>b</sup>The sample was positive biased with dc 60 V.

samples. The substrate was floated in the plasma with a floating potential of -5 to -10 V for samples 1–6. As seen from Table I, the etch rates are 0, 20, and ~1500 nm/min for pure O<sub>2</sub>, Ar, and CF<sub>4</sub> plasma, respectively. This proves that the O<sub>2</sub> plasma has no chemical etching effect to the As<sub>2</sub>S<sub>3</sub>, but the CF<sub>4</sub> plasma has a very strong chemical etch to the As<sub>2</sub>S<sub>3</sub>. The etch rate by the CF<sub>4</sub> plasma was greatly reduced to 130 or 210 nm/min by feeding 70% Ar or O<sub>2</sub> gas, respectively, to the processing gas mixture, as demonstrated by the etch rates of samples 4 and 5 in the table.

It is reasonable for the pure O<sub>2</sub> plasma to have no chemical etch effect to the  $As_2S_3$ , since all the possible products  $(As_2O_3, SO_2, etc.)$  are not volatile at low temperature. In fact, the surface of the As<sub>2</sub>S<sub>3</sub> could be oxidized after the O<sub>2</sub>-plasma irradiation. As compared with sample 5 in Table I, the etch rate of sample 6 by  $CF_4/O_2$  plasma reduced from 130 to 20 nm/min in the first 2 min after its surface was preirradiated using the  $O_2$  plasma for 10 min. The etch rate of sample 6 was found to become normal (130 nm/min) again after the first 2-min-etching. This indicates that a more resistant layer to the CF4 plasma was formed on the surface of the As<sub>2</sub>S<sub>3</sub> film after the O<sub>2</sub> plasma irradiation. We believed that this layer was composed of the oxides of As<sub>2</sub>O<sub>3</sub> and  $SO_2$ , because that the  $O_2$  plasma is well known to be very effective to oxidize the surface of many solid materials, including GaAs,<sup>13</sup> Al,<sup>14</sup> and Si,<sup>15</sup> etc., and it is also know that the surfaces of solid As and S can even spontaneously oxidize in air.16

The low etch rate (20 nm/min) of pure Ar plasma for sample 2 in Table I was generated by a pure physical sputtering effect of the plasma. Ar is an inert gas, having no chemical etching effect, but Ar ions are much heavier than O ions, they can remove material via physical sputtering effect. Even though there was no rf power being applied to the substrate, there was still a total ion bombardment potential of  $\sim$ 35 V, contributed by a substrate floating potential of -10 V, and a plasma potential of +25 V. It was thus possible for the Ar ions to generate a physical sputtering effect to the As<sub>2</sub>S<sub>3</sub> film, which is a low-density and soft solid material. In addition, Ar ion bombardment is well know to be able to enhance the surface chemical etching effect of many solid materials exposed in fluorine or fluoride gases.<sup>17</sup> This could

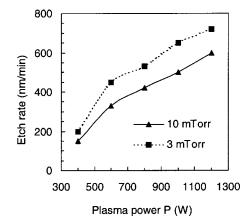


FIG. 6. Etch rate of the  $As_2S_3$  films vs the helicon plasma power *P*, with  $O_2/CF_4=7/3$ ,  $V_b=-100$  V, and pressure 3 or 10 mTorr.

be one of the reasons for a higher etch rate of the  $As_2S_3$  by the  $Ar/CF_4$  plasma than by the  $O_2/CF_4$  plasma at the same gas ratio, as seen from the etch rates of samples 4 and 5 in Table I.

In addition, the possibility and degree of the chemical etch to the As<sub>2</sub>S<sub>3</sub> induced by the neutral reactive species  $(F, CF, CF_2, CF_3)$  in the O<sub>2</sub>/CF<sub>4</sub> plasma was also checked. We applied a positive dc bias of 60 V to the substrate to repel all the positive ions, and to attract only electrons coming from the plasma. A etch rate of ~100 nm/min was obtained in this case as seen in Table I for sample 7. This etch rate is only a little bit lower than that (130 nm/min) of sample 5 being etch with a total ion bombardment potential of  $\sim 30$  V. This indicates that the chemical etch by the neutral species in the O<sub>2</sub>/CF<sub>4</sub> plasma plays a major role for etching the  $As_2S_3$ . The chemical etch by the neutral species could be enhanced by ion and electron irradiation to the surface of the As<sub>2</sub>S<sub>3</sub> as observed for the surface chemical etch of other materials in fluorine based gases.<sup>17</sup> The main etching products of the As<sub>2</sub>S<sub>3</sub> in the CF<sub>4</sub> plasma could be arsenic fluorides  $(AsF_{x})$  and sulfuric fluorides  $(SF_{x})$ , since they are known to be volatile at room temperature.

The dependence of the etch rate on the helicon plasma power *P* is displayed in Fig. 6. The applied substrate bias  $V_b$ was -100 V,  $O_2/CF_4=7/3$ , and pressure 3 or 10 mTorr. The etch rate is seen to increase significantly from ~200 to over 700 nm/min when increasing *P* from 400 to 1200 W as for the case of the gas pressure of 3 mTorr. The increase of the etch rate with *P* can be explained by the increase of the plasma density and the dissociation ratio of the CF<sub>4</sub> gas, as indicated by the results in Figs. 1 and 4. The increase of the etch rate when reducing the processing gas pressure from 10 to 3 mTorr was also related to the increase of the plasma density, as evidenced in Fig. 3.

The etch rates of the As<sub>2</sub>S<sub>3</sub> as functions of the processing gas flow ratio of O<sub>2</sub>/CF<sub>4</sub> and Ar/CF<sub>4</sub> are depicted in Fig. 7. The applied *P* was 600 W, bias  $V_b$ -100 V, and pressure 10 mTorr. As shown Fig. 7, the etch rate of the As<sub>2</sub>S<sub>3</sub> is over 2000 nm/min with pure CF<sub>4</sub> plasma (at O<sub>2</sub>/CF<sub>4</sub>=0), but it decreases dramatically to a few hundred nm/min when in-

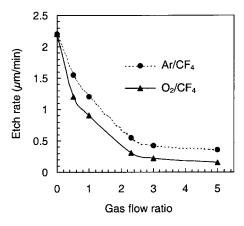


FIG. 7. Etch rate of  $As_2S_3$  as functions of  $Ar/CF_4$  and  $O_2/CF_4$  gas flow ratios, with a plasma power 600 W, substrate bias -100 V, and pressure 10 mTorr.

creasing the Ar/CF<sub>4</sub> or  $O_2/CF_4$  ratio to over 2/1; and a higher etch rate is generated using Ar/CF<sub>4</sub> than O<sub>2</sub>/CF<sub>4</sub> gas mixture at the same gas ratio. These results can be explained by the plasma-diagnosing results shown in Figs. 2 and 5. As concluded from Fig. 5, when increasing the  $Ar/CF_4$  or  $O_2/CF_4$  ratio to over 2/1, the concentrations of the atomic F and other reactive species in the plasma decreased greatly, and thus the etch rates decreased dramatically. In addition, the ion current density of Ar/CF<sub>4</sub> plasma is always higher than that of the  $O_2/CF_4$  plasma at the same gas ratio as showing in Fig. 2; and an Ar ion is much heavier than a O ion, making the Ar<sup>+</sup> has stronger bombardment effect than the O<sup>+</sup>. The ion bombardment not only produces physical sputtering effect, but also enhances the chemical etching effect of neutral reactants. These are some of the reasons for the higher etch rate of the  $Ar/CF_4$  than the  $O_2/CF_4$  gas mixture at the same gas ratio.

The etch rates of the Al mask as functions of the processing gas flow ratios of  $CF_4/O_2$  and  $CF_4/Ar$  are depicted in Fig. 8. The applied *P* was 600 W,  $V_b$ -100 V, and pressure 10 mTorr. As seen in Fig. 8, the etch rate of Al also decreases with the increase of the  $O_2/CF_4$  or  $Ar/CF_4$  gas flow

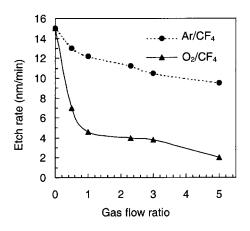


FIG. 8. Etch rate of Al mask layer as functions of  $Ar/CF_4$  and  $O_2/CF_4$  gas flow ratios, with plasma power 600 W, substrate bias -100 V, and pressure 10 mTorr.

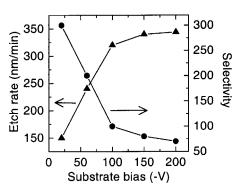


FIG. 9. Etch rate of  $As_2S_3$  and the etching selectivity of  $As_2S_3/Al$  vs the substrate bias  $V_b$  with  $O_2/CF_4=7/3$ , P=600 W, and pressure 10 mTorr.

ratio; and a much higher etch rate is generated using the  $Ar/CF_4$  than the  $O_2/CF_4$  gas mixture at the same gas ratio. In fact, Al is known to become oxidized quickly in air, especially in a  $O_2$  plasma,<sup>14,18</sup> so that a dense Al oxide (Al<sub>2</sub>O<sub>3</sub>) layer of 3–5 nm thick normally forms on the Al surface to prevent further oxidation of the Al. The Al<sub>2</sub>O<sub>3</sub> is also known to have very high resistance to the etch of the CF<sub>4</sub> plasma.<sup>14</sup> The addition of  $O_2$  to CF<sub>4</sub> gas was, therefore, of benefit in improving the resistance of the Al masks to CF<sub>4</sub>-plasma etching. Whereas, compared with the O<sub>2</sub> feeding, the Ar addition to CF<sub>4</sub> was in favor of intensifying the ion enhanced chemical etch and ion sputtering to the Al mask, leading to a quicker erosion of the Al mask.

The etch rate of the As<sub>2</sub>S<sub>3</sub> and its etching selectivity relative to the Al mask are depicted in Fig. 9 as functions of the substrate bias ( $V_b$ ). The applied P was 600 W, processing gas ratio O<sub>2</sub>/CF<sub>4</sub>=7/3, and pressure ~10 mTorr. This figure shows that the As<sub>2</sub>S<sub>3</sub> etch rate increases quickly with  $V_b$ when  $-V_b < 100$  V, and then it becomes near saturated at higher bias. The increase of the etch rate with the bias is generally caused by the enhancement of ion bombardment effect.<sup>19</sup> Figure 9 also shows that the As<sub>2</sub>S<sub>3</sub>/Al etch selectivity deceases with  $V_b$ , but a very high As<sub>2</sub>S<sub>3</sub>/Al selectivity of ~80–100 is still obtained in the bias range of -100 to -150 V. This is very important for achieving vertical waveguide sidewalls, and for accurate control of the waveguide width.

## C. Profile of the etched waveguides

Figure 10 illustrates the micrographs of the As<sub>2</sub>S<sub>3</sub> waveguides etched under different  $O_2/CF_4$  plasma conditions. The  $O_2/CF_4$  gas flow ratio was found to be one of the main parameters influencing the amount of undercutting. A serious undercut of more than 1.0  $\mu$ m could be generated for a 3  $\mu$ m thick waveguide if pure CF<sub>4</sub> plasma was applied, and a strong undercut of ~0.8  $\mu$ m for the 3  $\mu$ m thick waveguide occurred even when the CF<sub>4</sub> was diluted with 50% O<sub>2</sub>, as for the waveguide shown in Fig. 10(a), which was etched with  $O_2/CF_4=1:1$ , P=600 W, and  $V_b=-120$  V. The degree of undercutting was reduced to ~0.12  $\mu$ m when increasing the  $O_2/CF_4$  ratio to 7:3 whilst keeping other plasma parameters constant, as for the waveguide shown in Fig. 10(d).

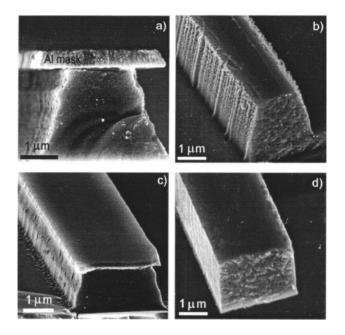


FIG. 10. Micrographs of the As<sub>2</sub>S<sub>3</sub> waveguides obtained using different etching condition: (a)  $O_2/CF_4=1/1$ , P=600 W, and  $V_b=-120$  V; (b)  $O_2/CF_4=7/3$ , P=1000 W, and  $V_b=-120$  V; (c)  $O_2/CF_4=7/3$ , P=600 W, and  $V_b=-50$  V; (d)  $O_2/CF_4=7/3$ , P=600 W, and  $V_b=-120$  V. The processing pressure was 10 mTorr for all samples.

Another parameter affecting the etching anisotropy was the helicon plasma power P. The degree of undercutting was found to increase with P whilst keeping other plasma parameters constant, as illustrated in Fig. 10, where the sidewalls of the waveguides changed from near vertical [in Fig. 10(d)] to quite slanted [in Fig. 10(b)] when P was increased from 600 to 1000 W due to the undercutting effect.

The substrate bias also played an important role in determining the undercutting. As seen in Fig. 10, again holding other plasma parameters constant, the waveguide obtained using a low  $V_b$  of -50 V appeared to have a larger undercut of ~0.45  $\mu$ m [in Fig. 10(c)], compared with the waveguide [in Fig. 10(d)] obtained using a high  $V_b$  of -120 V. The undercut resulting from low bias is commonly observed in plasma etching of different materials, and it is related to inadequate ion bombardment, and/or to insufficient control of the directions of the ions.<sup>19</sup>

To explain the undercut caused by the low  $O_2/CF_4$  ratio or high plasma power, we need to consider the etching mechanisms. There are three basic plasma-etching mechanisms: physical sputtering, ion-enhanced chemical etching, and chemical etching.<sup>19</sup> The first 2 etching effects are directional, or anisotropic, and they will not cause undercutting if enough substrate bias is applied. The last etching effect, pure chemical etching induced by neutral reactants is an isotropic process, which is responsible for the undercutting. It has been proven by the results in Table I that neutral reactants in the  $O_2/CF_4$  plasma play a major role in etching the As<sub>2</sub>S<sub>3</sub>. This is the reason for the strong undercut observed for some of the waveguides displayed in Fig. 10. Therefore, in order to reduce the undercutting, the isotropic etch effect induced by the neutral species need to be greatly weakened, while the anisotropy etch effects should be enhanced. This requires to reduce the concentration of the neutral reactants, and to enhance the ion bombardment. The latter requirement was achieved simply by increasing the substrate bias, while the former was achieved by the dilution of the  $CF_4$  gas using  $O_2$ , and by the reduction of the plasma power, as demonstrated by the results shown in Fig. 10.

In fact, as seen in Figs. 4 and 5, the intensity of the F-line at 684.6 nm is actually very low ( $\sim 100$ ) under the plasma conditions of P=600 W and  $O_2/CF_4=7/3$ , compared with that ( $\sim$ 700) obtained at a higher power of 1200 W, or with that (~1200) of the pure CF<sub>4</sub> plasma (at  $O_2/CF_4=0$ ). Therefore the concentrations of the atomic F, as well as other neutral reactants, were relatively very low under the plasma conditions of P = 600 W and  $O_2/CF_4 = 7/3$ . This greatly limited the isotropic etching effect of the plasma to the sidewalls of the waveguides. On the other hand, the ion current density was seen not to change much with the variation of the O<sub>2</sub>/CF<sub>4</sub> ratio while holding other parameters constant, as evidence in Fig. 2. This allows the degree of ion bombardment not to change much when varying the  $O_2/CF_4$  ratio. As a result, the isotropic chemical etch was greatly limited while a relative strong anisotropic etch or ion-bombardment enhanced chemical etch was remained when increasing the O<sub>2</sub>/CF<sub>4</sub> ratio. Therefore, near vertical sidewalls of the waveguide [in Fig. 10(d)] were obtained with the optimized plasma conditions of P=600 W,  $O_2/CF_4=7/3$ , and  $V_b$ = -120 V.

There should be no polymer passivation layer formed on the sidewalls of the waveguides when using the  $CF_4/O_2$ plasma to etch the  $As_2S_3$ , since the  $O_2$  plasma is very effective to remove the polymer layer deposited from any carbon fluoride gases,<sup>20</sup> and the oxygen acts as scavenger of  $CF_r$ radicals, reducing the sources for the polymer formation. We have originally suspected that there could be an oxide layer formed on the sidewall of the waveguide, which might act as a passivation layer to inhibit the undercutting. However, this is proved to be unlikely. Although, an oxide layer can be generated on the As<sub>2</sub>S<sub>3</sub> surface in a pure O<sub>2</sub> plasma as indicated by the etching behavior of sample 6 in Table I, the oxide layer could not form in the O<sub>2</sub>/CF<sub>4</sub> plasma, as evidenced by the fact that a high etch rate of over 100 nm/min of the As<sub>2</sub>S<sub>3</sub> was observed in the  $CF_4/O_2$  plasma, even when the sample was floated or positive biased, as shown in Table I for samples 5 and 7. The etching process of the  $CF_4/O_2$ plasma might suppress the oxide formation process even on the sidewall surfaces, where only little or even no ion bombardment was received.

The sidewall roughness of the  $As_2S_3$  waveguides was found to mainly come from the side etching effect of the plasma, besides from the edge roughness of the original Al mask patterns. As shown in Fig. 10, very rough sidewalls were obtained as long as a big undercutting was present, as for those shown in Figs. 10(a)-10(c). Whereas, smooth sidewalls were obtained when the undercutting was greatly reduced as for the waveguide shown in Fig. 10(d). The sidewall roughness of the waveguides shown in Figs. 10(a)-10(c) was over ~150 nm, as determined using the FESEM, but it was below 50 nm for the waveguide shown in Fig. 10(d). Reducing the roughness of the sidewalls is very important for the waveguide fabrication, since a rough surface causes significant scattering loss from the waveguide.<sup>21</sup>

#### **IV. SUMMARY**

In summary, plasma etching to  $As_2S_3$  thin films for waveguides fabrication in a helicon plasma reactor has been studied. The plasma etching behaviors and mechanisms were explained base on the etching results, and on the characteristics of the plasma diagnosed using Langmuir probe and optical spectroscopy techniques.

The  $O_2$  plasma showed no chemical etching effect to the  $As_2S_3$ , but it could oxidize the surface of the  $As_2S_3$ . The Ar plasma had a strong sputtering effect to the  $As_2S_3$ . The  $CF_4$  plasma exhibited a too strong chemical etch to the  $As_2S_3$ , and had to be diluted for reducing the undercutting and side-wall roughness of the waveguides. The neutral reactants in the  $CF_4$  plasma play a major role in etching the  $As_2S_3$ , and their etching effect could be enhanced by ion bombardment.

Ar and  $O_2$  gases were compared as the additives to dilute the CF<sub>4</sub> processing gas. The  $O_2$  showed a better dilution effect than the Ar in reducing the etch rate of the As<sub>2</sub>S<sub>3</sub>, and an  $O_2/CF_4$  plasma generated a much lower erosion rate to the Al masks than a Ar/CF<sub>4</sub> plasma at the same gas flow ratio. A very high As<sub>2</sub>S<sub>3</sub>/Al etching selectivity of ~80–100 was obtained using the  $O_2/CF_4$  plasma even at a very high substrate bias of -100 to -150 V.

The dependence of the etch rate of the  $As_2S_3$  on the gas flow ratio, plasma power and substrate bias were measured. It was found that the etch rate decreased dramatically from over 2000 nm/min to a few hundred nm/min when the gas flow ratio of the Ar/CF<sub>4</sub>, or O<sub>2</sub>/CF<sub>4</sub> was increased from 0 to over 2. The etch rate also shown to decrease significantly when reducing the plasma power or substrate bias.

Serious undercutting and very rough sidewall occurred when there was a strong isotropic etch, or insufficient substrate bias was applied. The isotropic etch process were greatly limited by reducing the concentrations of neutral reactants in the plasma through a heavy dilution of the  $CF_4$  gas using  $O_2$  addition, and through the reduction of the plasma power.  $As_2S_3$  waveguides with near vertical and very smooth sidewalls were obtained using an optimized  $CF_4/O_2$  plasma with a flow ratio of  $O_2/CF_4=7/3$ , plasma power 600 W, substrate bias -120 V, and processing gas pressure  $\sim 10$  mTorr.

Although, some guidelines and understandings are present in this paper for the plasma etching of the  $As_2S_3$  thin films, further studies are however still required to improve the etching results, and to clarify the etching chemistry.

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