Beam oscillations and curling in chirped periodic structures with metamaterials

Arthur R. Davoyan, Andrey A. Sukhorukov, Ilya V. Shadrivov, and Yuri S. Kivshar
Nonlinear Physics Center, Research School of Physics and Engineering, Australian National University, Canberra ACT 0200, Australia
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We study the propagation of electromagnetic waves in one-dimensional chirped periodic structures composed of alternating layers of negative-index (or left-handed) metamaterial and conventional dielectric, under the condition of the zero average refractive index. We consider the case when the periodic structure has a linear chirp, and the chirp is introduced by varying linearly the thickness of the layers across the structure. We apply an asymptotic analytical method for the analysis of the Bloch oscillations and find that, in a sharp contrast to ordinary periodic dielectric structures, the energy flow in multilayered stacks with metamaterials may have the opposite direction at the band edges, thus providing possibilities for the beam steering in the transmission band.

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I. INTRODUCTION

Materials with negative index of refraction, also known as left-handed metamaterials, are attracting a great scientific interest nowadays. This type of materials was predicted theoretically back to 1967 [1] but only 30 years later this theoretical curiosity was followed by the first experimental demonstrations based on the fabrication of composite structures consisting of split-ring resonators and metallic wires [2,3]. The basic properties of the left-handed metamaterials predicted theoretically have been confirmed by experiment, and this led to a rapid progress in this field and many other interesting discoveries. In particular, many new physical phenomena based on the concept of metamaterials and negative index of refraction have been predicted, including the fundamental concept of perfect lens [4] and, more recently, electromagnetic cloaking [5–7].

One of the interesting directions in the analysis of the unusual properties of this composite metamaterials is the study of periodic structures (or photonic crystals) composed of metamaterials. Photonic crystals, being widely used for both light control and beam manipulation, demonstrate a variety of physical effects, and they may offer many new possibilities being combined with metamaterials. In particular, a series of recent studies revealed the existence of zero-index band gaps [8–11] associated with one-dimensional photonic crystals composed of alternating layers of negative-index and conventional dielectrics for which the averaged refractive index vanishes. Such periodic structures demonstrate many intriguing properties, including substantial suppression of the Anderson localization and long-wavelength resonances [12].

In this paper, we study the propagation of electromagnetic waves in one-dimensional periodic structures composed of alternating layers of left-handed metamaterial and conventional dielectric. It is well established [13,14] that introducing a chirp into a one-dimensional periodic structure leads to the generation of optical Bloch oscillations which can be also predicted in the presence of metamaterials [15]. In addition to our numerical analysis of the Bloch oscillations studied earlier [15], in this paper we demonstrate a number of unique features of the beam propagation in this kind of chirped periodic composite structures. In particular, in contrast to Ref. [15], here we consider the chirped structures with a large number of layers and slowly varying period. Applying the approximation based on the geometric optics, we reveal a variety of effects that could be observed in such structures, including the reversal of the energy flow at the band edges and the fascinating effect of the beam curling. This effect of the beam curling can be useful for the beam steering in the transmission band. We also study the eigenvalue problem and the corresponding eigenmodes and determine both the field structure and Poynting vector distribution associated with the beam propagation.

The paper is organized as follows. In Sec. II we introduce our structure as a one-dimensional stack of layers composed of alternating layers of metamaterial and dielectrics. We discuss the way of presenting eigenmodes of the structure with a slowly varying period and discuss the initial conditions. In Sec. III we implement the Bloch theorem and derive the dispersion relation for the Bloch wave vector. Then, we analyze the band-gap diagram for this structure and discuss the conditions for the observation of a type of the beam dynamics associated with the Bloch oscillations. Section IV is devoted to the geometric optics approximation. Here we demonstrate a possibility to apply the geometric optics for the analysis of layered structures with slowly changing parameters. We derive the equations of motion for the paraxial beams, and also study the period of oscillations pointing out properties of the beam trajectories connected with a change of the sign of the spatial group velocity in the structure due to the presence of a metamaterial. Also, we analyze different regimes of the beam propagation and compare them with the well-known case corresponding to the similar structures composed of conventional dielectric layers. In Sec. V, we discuss the eigenvalue problem and point out the difficulties and failure of the commonly used numerical techniques. In addition, we describe an alternative method to find the eigenmodes of the structures with a large number of periods. Based on this method, we study the field distribution in the structure and determine the direction of the Poynting vector in the beam. We observe a close correspondence with predictions of the geometric optics. Finally, Sec. VI concludes the paper.
II. STRUCTURE GEOMETRY AND EIGENMODE FORMALISM

We study a one-dimensional chirped periodic structure shown schematically in Fig. 1, where the slabs of a negative-index metamaterial with the width $d_m$ are separated by the layers of the conventional dielectric with the width $d_m$. We describe the variation of the refractive index in the $m$th pair of layers as follows:

$$\begin{align*}
n(z) &= \begin{cases} 
n_r = \sqrt{\varepsilon_r \mu_r}, & z \in (z_m, z_m + d_m), \\
n_i = -\sqrt{\varepsilon_i \mu_i}, & z \in (z_m + d_m, z_m + \Lambda_m),
\end{cases}
\end{align*}$$

where $n_i$ and $n_r$ are the refractive indices of metamaterial and dielectric layers, respectively, $\Lambda_m$ is the width of the $m$th unit cell. In contrast to our previous studies [15], here we analyze the structures with a large number of unit cells and slowly varying period.

We consider TE-polarized waves with the electric field described by one component $E_x = (E_x, 0, 0)$, and the waves propagating in the $(y, z)$ plane. In this case the problem is described by the Helmholtz equation,

$$\Delta_x E_x(y, z) + n(z)^2 E_x(y, z) - \frac{1}{\mu} \frac{d \mu(z)}{dz} \frac{\partial E_x(y, z)}{\partial z} = 0,$$

where $\Delta_x$ is the two-dimensional Laplacian. The field is assumed to be monochromatic with the frequency $\omega$, and the coordinates are expressed in the units of $c/\omega$, $c$ is the speed of light.

For the structures with slowly varying periods, the eigenmodes of the problem (2) can be introduced by applying the Bloch theorem for periodic systems and the corresponding Bloch-wave formalism [16]. In this approach, the electric field corresponding to the eigenmode with the propagation constant $k_z$ in the unit cell with the width $\Lambda$ can be represented as

$$E_A(z, y) = A_A U_A(z) \exp[-i(K_A z + k_0 y)],$$

where $k_0$ and $K_A$ are normalized to $\omega/c$, the amplitude $A_A$ varies slowly across the structure, $U_A$ is the Bloch function, and $K_A$ is the Bloch number of the periodic structure with the unit cell size $\Lambda$, which we analyze systematically in Sec. III.

We now analyze the dynamics of beams. The beam can be launched with near normal incidence at the structure termination along the $z$ axis, with the input location corresponding to the transmission band. Whereas we do not analyze the excitation process, the field distribution away from the boundaries can be represented as a superposition of eigenmodes of an infinitely extended structure. In order to reveal the generic aspects of beam dynamics, we suppose that at some plane $y = 0$, located inside the structure, we have electric field distribution defined as

$$E(y, z) = \exp[-(z-z_0)^2/h] E(z) = \psi(z) E(z),$$

where $E(z)$ is the eigenmode of Eq. (3) with the propagation constant $k_z = k_0^b$, which will determine propagation direction; $h$ is the beam width, which we consider to be significantly large, i.e., $h \gg (\Lambda)$. The field in the structure can be represented as a superposition of eigenmodes. As long as the Gaussian beam is wide with respect to the unit cell, the spectrum of the contributing eigenmodes is narrow, and it is centered near the point $k_0^b$ [16]. Such beam can be treated within the paraxial approximation. The beam propagation is mainly described by the modes with $k_z \approx k_0^b$ and the tangent of the beam angle is defined by $\partial k_z/\partial K_0 |_{k_z = K_0} = k_0^b$, where $K_0$ corresponds to the beam launching point. An additional beam tilt can be introduced in a more general case of complex $\psi(z)$.

III. PERIODIC STRUCTURE: BAND-GAP PROPERTIES

As the first step of our analysis, we study the periodic structure with the period $\Lambda$ without a chirp. In this case, Eq. (2) has periodic coefficients, and we can apply the Bloch theorem [17] and present the electric field in the form

$$E_x(z, y) = U(z) \exp[-i (K_0^b z + k_0^b y)],$$

where $K_0$ is the Bloch number, and the field envelope $U(z)$ is a periodic function with the period $\Lambda$, so that $U(z+\Lambda) = U(z)$. In the $m$th pair of layers, the Bloch waves are presented as

$$U_{lm}(z) = \{a_{lm} \exp[-ik_{z,l}(z-m\Lambda)] + b_{lm} \exp[iK_0^b(z-m\Lambda)]\} \exp[iK_0^b(z-m\Lambda)],$$

where the indices $l$ and $r$ correspond to the left- and right-handed slabs, respectively, and the amplitudes $a_{lm}$ and $b_{lm}$ are found from the boundary conditions at the interfaces separating the metamaterial and dielectric layers (see, e.g., Refs. [16–18]). The Bloch wave number $K_0$ is defined from the dispersion relation...
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FIG. 2. (Color online) Left-hand side: Bloch-wave phase incursion in the transmission regime for different values of the propagation constant $k_y$. Inset shows a magnified part of the plot with the mode crossing. Middle: Band-gap diagram for $e_l=\mu_l=1$, $d_{lm}/d_{ln}=2$ and $e_l=-5$, $\mu_l=-0.8$; low-order transmission resonance is shown. Right-hand side: Group velocity $\partial k_y/\partial k_b$ for different values of the propagation constant.

\begin{equation}
2\cos(K_y\Lambda) = 2\cos(k_{y,d_l})\cos(k_{y,d_l}) - \left(\frac{k_{y,d_l}\mu_l}{k_{y,d_l}\mu_l}\right)\sin(k_{y,d_l})\sin(k_{y,d_l}),
\end{equation}

where $k_{y,d_l}=\frac{\sqrt{n_{d_l}}}{\Lambda}$ and $k_y$ is the propagation constant along the $y$ axis.

According to Eq. (5), the waves can propagate in the structure when $K_y$ is real. In Fig. 2 (middle), we plot the band-gap diagram of the layered structure on the plane $(\Lambda, k_y)$. Here we assume that the dielectric layer is air, $e_r=\mu_r=1$, and the dielectric layers are 2 times thicker than the metamaterial layers, i.e., $d_{lm}/d_{ln}=2$, and this ratio is preserved across the structure. We choose the metamaterial with the parameters $e_r=-5$ and $\mu_r=-0.8$.

The band-gap properties of one-dimensional periodic structures with metamaterials have been studied in several papers [10,11], including the case of the zero-index averaged refractive index [9]. It was shown that for the structures with $\int n(z)dz=0$ the band-gap spectrum includes transmission resonances which shrink into infinitesimally thin lines into a complete band gap when the widths of the slabs coincide [9]. For the normal incidence (i.e., when $k_z=0$), the transmission is observed only when $n_{d_l}=n_{d_l}=\pi q$, where $q$ is integer.

We study the Bloch wave phase incursion $K_y\Lambda$ across the structure for different values of the propagation constant $k_y$, see Fig. 2 (left-hand side). For small values of the propagation constant (e.g., $k_y<0.5$), the low-order transmission resonances have zero phase incursion, in contrast to the case of conventional dielectric Bragg gratings. The maximum of the phase is accumulated in the middle of the transmission band, and its amplitude increases with the increase of the band order, reaching the value of $\pi$ in the higher-order transmission resonance. A growth of the propagation constant leads to the band coupling $(0.5\leq k_y\leq 1)$, not shown here. The phase incursion in a new coupled broadband region is approaching $\pi$. Further increase of the propagation constant leads to the narrowing of the transmission regions and to a rapid increase of the phase across the band to the value of $\pi$. On the band-gap diagram, we observe two turning points at $k_y=1.7$ and $k_y=2$ [marked points 1 and 2 in the inset of Fig. 3 (middle)]. At these points the modes with close $k_y$ have the same value of the Bloch wave number near the band edge. We trace the behavior of the band edges $\xi_r(k_y)$ and $\xi_t(k_y)$ with a change of the propagation constant $k_y$. For $k_y=1.7$, the left band edge $\xi_r$ changes the type of its monotonicity. Consequently, in this region the left ($\xi_r$) and right ($\xi_t$) band edges have different slopes, i.e., $(\partial \xi_r/\partial k_y)(\partial \xi_t/\partial k_y)<0$, as shown in the inset of Fig. 3. The latter, with consideration

FIG. 3. (Color online) Left-hand side: Period of beam oscillations. Inset shows the region of the sign change. Middle: Band-gap diagram. Inset shows the turning points. Right-hand side: Spectrum of the beam centered at the point $k_y^0=1.843$.

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that phase is growing from 0 to \( \pi \) in the transmission region, leads to the crossing of the corresponding modes (see inset in Fig. 2). Finally, for \( k_y = 2 \), the right band edge \( \zeta_y \) also changes the sign of its slope, and \((\partial \zeta_y/\partial k_y)(\partial \zeta_y/\partial k_x)\) becomes positive. We note that for small values of \( k_y \), the first-order band edges also have different signs of their slopes but a new type of behavior cannot be observed because the phase incursion vanishes in the band for \( k_y < 0.5 \). Also, in the conventional Bragg gratings both band boundaries have the same slope and thus the mode crossing does not occur.

Crossing of two modes means that the effective spatial velocity defined as \( v = \partial k_x / \partial k_y \), has different signs at different sides of the crossing point, and it becomes singular at the phase. As long as the velocity is related to the energy flow, we observe different directions of the energy flow in the \( y \) direction at different edges of the band, as will be discussed in more details in Sec. IV and Sec. V. We plot the velocity for different values of the propagation constant \( k_y \), see Figs. 2(a)–2(c). For \( k_y \) outside the region, Fig. 2(a), the velocity does not change its sign in the band, thus meaning that energy flow has the same direction at any point of the band. Similar type of the beam evolution can be found in the stacks of conventional dielectric layers. Further increase of \( k_y \) leads to more asymmetric velocity profile and, finally, at \( k_y = 1.7 \) [see Fig. 2(b)], the velocity becomes infinite at the left band edge. In Sec. IV we demonstrate that this case corresponds to the energy flow vanishing in the \( y \) direction. When the propagation constant \( k_y \) is inside the region [see Fig. 2(c)], the velocity profile has the second-order discontinuity with the sign changed inside the band. Consequently, the energy flow in the \( y \) direction also changes its sign within the transmission band. The singularity point in the spatial velocity profile moves from the left band edge to the right band edge with the growth of the propagation constant from \( k_y = 1.7 \) to \( k_y = 2 \), (see turning points 1 and 2 in Fig. 3). Finally, for the propagation constants \( k_y > 2 \), the velocity profile becomes continuous and negative, indicating that the waves are backward in the whole band.

Below, we consider the simplest case of a linear chirp of the structure, \( \Lambda_{0}+\delta \Lambda \) with \( \delta \Lambda \ll \Lambda \), see Fig. 1. For \( \delta \Lambda \rightarrow 0 \), i.e., an adiabatic change of the unit cell size across the structure, we implement the geometric optics approximation.

### IV. GEOMETRIC OPTICS APPROXIMATION

We study the evolution of the Poynting vector by employing an analogy with a homogeneous medium having gradually changing refraction index \([18,19]\). We consider the time-averaged Poynting vector,

\[
S = \frac{c}{8\pi} \text{Re}[E \times H^*] = -\frac{c}{8\pi\mu} \text{Re} i \left( e_y E_y \frac{\partial E_x^*}{\partial z} + e_z E_z \frac{\partial E_x^*}{\partial y} \right),
\]

where \( E_x \) is given by Eqs. (4), \( e_x \) and \( e_y \) are the unit vectors.

The time-averaged electromagnetic energy density is defined as

\[
\langle S \rangle = \frac{1}{16\pi} \text{Re}(\varepsilon E E^* + \mu H H^*)
\]

\[
= \frac{1}{16\pi\mu} \text{Re} \left( \varepsilon \mu |E_x|^2 + \left( \frac{\partial E_x}{\partial z} \right)^2 + \left( \frac{\partial E_x}{\partial y} \right)^2 \right).
\]

In a homogeneous medium, the time-averaged Poynting vector is tangential to the beam trajectory. It changes gradually with continuously varying refractive index, thus defining a geometric ray. In our case, the Poynting vector changes its direction stepwise within each unit cell, since the refractive indices of the slabs comprising the unit cell have the opposite signs. To describe an average behavior of the energy flow on a larger scale, we consider the Poynting vector and energy density averaged over the unit cell, \( (\langle S \rangle) = \frac{1}{N} \int S dz \) and energy density \( \langle w \rangle = \frac{1}{N} \int w dz \), respectively.

We introduce the average velocity of the energy flow \([16,17]\):

\[
\mathbf{v}_e = \frac{\langle S \rangle}{\langle w \rangle}. \tag{10}
\]

As long as the width of the unit cell changes adiabatically across the structure, the average velocity of the energy flow \( \mathbf{v}_e \) changes quasicontinuously. Therefore, we can define the rays in the space \((\Lambda, y)\) (we note here that due to the linear chirp of the structure, the spatial coordinate \( z_m \) is a linear function of \( \Lambda \) as trajectories along which the average energy \( \langle S \rangle \) is directed. Thus, the ray equation is defined as follows:

\[
\frac{dr}{dt} = \mathbf{v}_r, \tag{11}
\]

where \( r = e_y y + e_z \Lambda \) is the radius-vector describing the ray, \( t \) is the time in units of \( \omega^{-1} \), \( \omega \) is the angular frequency.

In Ref. [16] it was shown that for a paraxial beam the average velocity of the energy flow coincides with the group velocity defined as

\[
\mathbf{v}_e = \mathbf{v}_g = \nabla_K \omega = \frac{\partial \omega}{\partial \mathbf{K}}, \tag{12}
\]

where \( \mathbf{K} = e_y k_y + e_z K_z \) is the wave vector, and \( \omega \) is the angular frequency.

For a fixed frequency \( \omega \) of monochromatic beam we obtain the dispersion relation \( k_x = f(K_x) \) [see Eq. (7)], corresponding to the curve in the space \((k_y, K_x)\) described by the wave vector \( \mathbf{K} \), which is analogous to the equifrequency surface for anisotropic media \([20]\). Consequently, using Eqs. (10)–(12) we obtain \( \mathbf{v}_e = \mathbf{v}_g \) and \( \langle S \rangle \) is normal to the curve \( k_x = f(K_x) \). The latter condition is described by the equation

\[
\frac{\langle S_y \rangle}{\langle S_z \rangle} = -\left( \frac{\partial k_x}{\partial K_y} \right)^{-1} = -\frac{1}{\nu}, \tag{13}
\]

where \( \langle S_y \rangle \) and \( \langle S_z \rangle \) are the \( y \) and \( z \) components of the Poynting vector \( \langle S \rangle \), \( \nu \) is the spatial velocity of the ray.

Relation (13) between the Poynting vector components and velocity \( \nu \) shows that when \( \nu \to \infty \), \( \langle S_y \rangle = 0 \), and the total energy flows along the \( z \) direction. On the other hand, when \( \nu = 0 \), the energy flows along the structure \( \langle S_z \rangle = 0 \).

Using Eqs. (9) and (12), we rewrite Eq. (11) as follows:
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from the Fermat principle. We multiply Eq. using Eq. \( H \).

The Hamilton equations for the rays can be derived in general suggestions, assuming that \( k_y \) refers to the “energy,” being preserved in the structure and \( \partial k_y / \partial K_b \) being the “group velocity” of the paraxial beam.

The first equation of the system (17) describes diffractionless motion of a beam with a narrow spectrum centered near the point \( k^0_y \). The beam motion is equivalent to the motion of an effective particle in a one-dimensional potential \( W = \frac{1}{2} \nu^2 \phi \) between left \( \zeta_- \) and right \( \zeta_+ \) band edges. As long as the spectrum of allowed energies near the point \( k^0_y \) is quasicontinuous for infinite structures with adiabatically changing width \( \Lambda \), the motion remains periodic with the period of oscillations \( \Phi \) found as

\[
\Phi(k_y) = 2 \int_{\zeta_-}^{\zeta_+} \frac{d\Lambda}{\nu(\Lambda, k_y)},
\]

where \( \zeta_- \) and \( \zeta_+ \) refer to the band edges, \( \nu \) is defined by Eq. (13). In the gap regions, the field decays exponentially across the structure so that the motion is prohibited, and the spatial velocity vanishes at the band edges. Consequently, the expression under the integral has singular points at \( \zeta_- \) and \( \zeta_+ \) and the integration fails. To resolve this problem, we introduce a new variable \( \xi \),

\[
\Lambda = \frac{\xi - \xi_+}{2} + \frac{\xi - \xi_-}{2} \cos(\xi),
\]

and obtain

\[
\Phi = 2 \int_0^\pi \frac{(\xi - \xi_-) \sin(\xi)}{2} \frac{d\xi}{\nu(\xi, k_y)}.
\]

The expression under the integral is finite within the integration boundaries, hence the new integral is converging. Using the integral (20) we calculate the dependence of the period on the propagation constant \( k_y \), see Fig. 3 (left-hand side).

We observe that with a growth of \( k_y \), the oscillation period grows as well, this is explained by broadening of the band described in Sec. II. A further increase of \( k_y \) leads to the band narrowing and decrease of the oscillation period \( \Phi \). For \( 1.7 < k_y < 2 \), i.e., between the turning points, the period vanishes meaning that the corresponding mode does not transfer energy along the structure. A further increase of \( k_y \) leads to negative values for the period of oscillations, which corresponds to the total energy flow in the direction opposite to the propagation constant \( k_y \).

Using Eq. (17) and Eq. (20), we calculate the beam trajectories. First, we verify our results for the well-known structures with conventional dielectric slabs, and the trajectory corresponding to this case is shown in Fig. 4 (left-hand side).
side). We assume that a dielectric layer with the width $b$ has the parameters $\varepsilon_b=10$ and $\mu_b=1$, and the layers are separated by vacuum of the width $a$, so that $a/b=2$. We reveal a close correspondence between our results and the trajectories calculated by means of the geometric optics in Ref. [14]. The beam is reflected from both band boundaries, where the spatial velocity vanishes. The total energy flow along the $y$ direction is positive, and it preserves its sign during oscillations. For the structures with metamaterials, the beam with the spectrum centered near the propagation constants $k_y$ outside of the region between turning points (points 1 and 2 in Fig. 3) experiences the same reflection from the boundaries of the Brillouin zone with the total energy flow along the structure in the positive direction, for $k_y<1.7$, and in the opposite (negative) direction, for $k_y>2$.

Next, we study the beam propagation for the values of $k_y$ inside the region between the turning points. The trajectory calculated near the first turning point (see Fig. 4) has a peculiarity near the left band edge. Corresponding period of oscillations is shown in Fig. 3 (left-hand side). Near the left band edge the group velocity becomes infinite, thus energy flow along the layers vanishes, and the energy flow across the structure changes its sign. Hence a vortex structure is formed at this point. The observed spike is formed by narrowing of the trajectory near the left band edge with increase of propagation constant until it reaches the first turning point. Further increase of propagation constant, as was described in Sec. II, corresponds to a shift of the singular point of the group velocity further into the band region. The trajectories corresponding to this case are shown in Figs. 4(a)–4(e). Since the group velocity changes its sign before and after the singular point, the trajectory crosses itself and a beam curl is formed. For $k_y^0=1.85$ we observe a curl near the left band edge of the structure, see Fig. 4(b). Further increase of the propagation constant leads to the increase of the curl’s size, and decrease of the period, see Fig. 3. Finally, at $k_y^0=1.895$ the curl reaches the other transmission band edge forming a practically closed trajectory with almost zero period of oscillations, see Fig. 4(e). Note that near the left band edge the energy flow in the $y$ direction is negative but remains positive near the right band edge. Further increase of the wave-number results in the opposite process with the curl forming near the right band edge, see Fig. 4(d). For the propagation constants $k_y$ corresponding to the second turning point the curl vanishes, with a spike forming near the right band edge, and the total energy flow along the structure is in the opposite direction to the propagation constant. For $k_y^0>2$, the spike vanishes, and smooth reflection from the right band edge is formed. The trajectory again becomes continuous and without any ambiguities.

V. NUMERICAL SIMULATIONS

For the finite structures with nonadiabatic change of the unit-cell size, the approximation of geometric optics is not valid, however we can still apply the Bloch-wave formalism for describing the beam propagation, including the beam diffraction and formation of interference patterns. To find the field distribution in the structure, we calculate the eigenmodes $E(z)$ and eigenvalues $k_y^0$ of a finite stack of layers. There are several known approaches to solve this problem. The first approach is based on the representation of the field in each slab in the form of the counterpropagating waves. Boundary conditions between the layers define the ratio of the corresponding wave amplitudes in the slabs. These amplitudes can be represented in terms of either transfer matrix or scattering matrix formalisms [17,21]. The transfer matrix approach can be used for calculating the eigenmodes and eigenvalues for the structures with a small number of periods, and it is not suitable for calculating evanescent modes in long structures. The scattering matrix approach provides a better convergence, but it also cannot be applied for calculating evanescent modes in the structures with more than approximately 100 slabs. Another approach is based on the discretization of the wave equation across the structure, and we have used it previously to find the eigenvalues of the discrete problem [15]. However, this approach is computationally intensive, and it is not practical for calculating the transmission of very long structures.

Here we implement another approach based on the Bloch wave formalism. In Sec. II we have already demonstrated that for the slowly varying period of the structure (i.e., $\delta A \ll \Lambda$) the eigenmodes can be described by Eq. (3) with the amplitudes $A_\lambda$ and wave numbers $k_y$. We assume that the structure with a linearly changing period is placed between two semi-infinite periodic structures, with the period coinciding with that of the adjacent layers of the structure, see Fig. 1. In each unit cell the field can be presented as a superposition of the forward and backward propagating Bloch waves,

$$E_\lambda(x,y,z) = A_\lambda U_\lambda(x) \exp[-i(K_{\lambda}x + k_y y)] + B_\lambda U_\lambda(x) \times \exp[-i(K_{\lambda}x + k_y y)],$$

where $A_\lambda$ and $B_\lambda$ are the slowly varying amplitudes, $U_\lambda$ and $K_{\lambda}$ are defined by Eqs. (6) and (7), respectively.

In the left semi-infinite structure, the fields decay exponentially, and we choose the amplitudes in the first layer as $A_\lambda=1$ and $B_\lambda=0$. In the right semi-infinite structure the forward wave vanishes, and this means that $A_\lambda=0$ and $B_\lambda=1$. We calculate the amplitudes in the adjacent unit cells using the boundary conditions. Repeating this procedure we find the amplitudes in the whole structure (for more details, see the Appendix). We note that $K_{\lambda}$ is real in the band, hence the Bloch waves are propagating, and the modes do not grow exponentially. In the layers adjacent to the band, $K_{\lambda}$ is imaginary and, consequently, the amplitudes grow exponentially. We choose a relatively small number of unit cells with the parameters corresponding to the band gap, so that the amplitudes $A_\lambda$ and $B_\lambda$ remain reasonable across the structure. We note that the absolute value of the ratio of the amplitudes of the counterpropagating waves in the band is unity, so that the energy is localized in the transverse direction inside the structure. We trace the dynamics of the Bloch wave amplitudes from left and right boundaries separately and compare the amplitudes in the middle of the band region, see Fig. 5. For the eigenmodes with the eigenvalues $k_y$, the amplitudes...
note that the pattern created by the forward and backward propagating waves. The field distribution is restored almost completely after the first period of oscillations.

The field distribution is restored almost completely after the distance \( ky = 1.838 \), see Fig. 5. It is clearly seen that at \( ky = 1.838 \), the initial field distribution is represented as a superposition of the eigenmodes, and the full structure of the fields can be retrieved.

We calculate the eigenmodes for the structure consisting of 2100 unit cells with the width changing linearly from the value \( \Lambda_y = 4.23 \) to the value \( \Lambda_y = 4.44 \), and \( \delta \Lambda = 2 \times 10^{-4} \). We note that \( \langle A \rangle = \frac{\lambda}{2} \), where \( \lambda \) is a free space wavelength. The width of the whole structure is approximately 1500\( \Lambda_y \), which is, e.g., about a few millimeters in the infrared regime. We have chosen the initial field distribution in the form of Gaussian beam, see Eq. (4), launched near the right band boundary of the structure, see Fig. 6. The width of the beam is \( a = 20(\Lambda_y + \Lambda_y)/2 \), i.e., with about 20 unit cells excited, \( k_0 = 1.838 \). We decompose the initial field distribution into the superposition of eigenmodes of the structure by the least-squares method. The spectrum of the excited eigenmodes is shown in Fig. 3 (right-hand side). The spectrum is narrow, and it is centered near \( k_y = 1.838 \). The spectrum is to some accuracy equidistant, meaning that the field restores its shape after the distance \( \Phi = 2 \pi / \delta k_y \). We plot the field amplitude averaged over the unit cell. The beam curling predicted in the framework of the geometric optics is clearly observed. At the beam self-crossing point we observe an interference pattern created by the forward and backward propagating waves. The field distribution is restored almost completely after the first period of oscillations.

Now we calculate the distribution and direction of the Poynting vector. In Fig. 7 we plot the Poynting vector averaged across the unit cells. It is clearly seen that near the left boundary the direction of the Poynting vector along the \( y \) axis is opposite to the direction near the right boundary. At the self-crossing point corresponding to singularity of the group velocity, we observe that the energy flow vanishes in the \( y \) direction.

We also calculate the average \( y \) component of the Poynting vector, defined as \( \langle S_y \rangle \), on the unit cell and show its dynamics across the structure for the mode with the propagation constant \( k_y = 1.838 \), see Fig. 5. It is clearly seen that at the left boundary of the band the energy flow direction is opposite to that near the right boundary, and it vanishes in the center of the structure. This dynamics is consistent with the behavior predicted within geometric optics approximation in Secs. II and IV. We note that the total energy flow, i.e., the integrated flow across the structure, remains positive for this mode and for all modes contributing to the beam spectrum.

FIG. 6. (Color online) Distribution of the averaged field amplitude in the structure, for the beam with the width \( a = 20 \Lambda_y \), at \( k_0^z = 1.838 \). Oscillation period is about 2350.

FIG. 7. (Color online) Distribution of the averaged field amplitude and Poynting vector in the chirped structure. Arrows show the direction of the energy flow.
VI. CONCLUSIONS

We have presented a systematic analysis of the propagation of electromagnetic waves in chirped periodic structures composed of two kinds of alternating layers, the layers of negative-index metamaterial and the layers of conventional dielectrics, under the condition of the zero averaged refractive index. We have considered the chirp in the structure parameters introduced by varying the thickness of all layers linearly across the structure, and we have applied the methods of the geometric optics for analyzing the beam propagation and Bloch oscillations in such infinite composite structures. For the adiabatically changing period of structure, we have predicted the beam self-crossing in the bands, and have found that the energy flow in such multilayer structures with metamaterials may have the opposite direction at the band edges, in a sharp contrast to the similar structures composed of conventional dielectrics. This effect of the beam curling can be useful for the beam steering in the transmission band.

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APPENDIX

In this Appendix we discuss the relation between the Bloch amplitudes $A_m$ and $B_m$ for the $m$th layer and the amplitudes $A_0$ and $B_0$ in the 0th layer.

We describe the field in the $m$th unit cell of the periodic structure with the period $A_m$ as a Bloch wave $E_m(z, y)$ composed of the counterpropagating components with the amplitudes $A_m$ and $B_m$, see Eq. (21). We consider the boundary between $m$th and $(m+1)$th unit cells, i.e., $z=z_{m+1}$, see Fig. 1. The boundary condition at this interface requires that

$$E_m(z_{m+1}) = E_{m+1}(z_{m+1}),$$

$$\frac{1}{\mu_i} \frac{\partial E_m(z)}{\partial z} \bigg|_{z_{m+1}} = \frac{1}{\mu_r} \frac{\partial E_{m+1}(z)}{\partial z} \bigg|_{z_{m+1}}. \quad (A1)$$

Substituting Eq. (3) into Eq. (A1), we obtain

$$A_m(a_i^+ + b_i^-) + B_m(a_i^- + b_i^+) = A_{m+1}(a_i^+ e^{ik_A} + b_i^- e^{-ik_A}) e^{-ik_A} + B_{m+1}(a_i^- e^{ik_A} + b_i^+ e^{-ik_A}) e^{ik_A},$$

$$k \frac{A_m(a_i^- - b_i^+) + B_m(a_i^+ - b_i^-)}{\mu l} = k \frac{A_{m+1}(a_i^+ e^{ik_A} - b_i^- e^{-ik_A}) e^{-ik_A}}{\mu r} + B_{m+1}(a_i^- e^{ik_A} - b_i^+ e^{-ik_A}) e^{ik_A} \quad (A2)$$

where $\pm$ corresponds to the forward and backward propagating Bloch waves, respectively. Equation (A2) can be presented in the matrix form

$$D_m \begin{pmatrix} A_m \\ B_m \end{pmatrix} = D_{m+1} \begin{pmatrix} A_{m+1} \\ B_{m+1} \end{pmatrix}. \quad (A3)$$

Using this matrix equation, we can present the field amplitudes at the $m$th layer through the corresponding amplitudes at the 0th layer,

$$\begin{pmatrix} A_0 \\ B_0 \end{pmatrix} = \left( \prod_{i=1}^{m} D_i^{-1} D_{r} \right) \begin{pmatrix} A_m \\ B_m \end{pmatrix}. \quad (A4)$$